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Temperature Coefficients of Elastic Constants of Quartz

by

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We have reported in the paper (JIEE Japan, Vol. 54, No. 543, p.940, Oct. 10, 1933 on October 1933) on the thickness vibration of quartz oscillating plates cut in parallel to X-axis (Figure 1) that the vibration mode is sharing vibration and frequency is expressed as

$$f = \frac{q}{2a} \sqrt{\frac{c}{\rho}}, \quad c = \frac{1}{2}(c_{11} - c_{12}) \sin^2 \theta + c_{44} \cos^2 \theta - c_{14} \sin 2\theta \quad \text{----- (1)}$$

Based on the equation (1), we estimated that temperature coefficients of oscillation would change along with the change of θ and we reported the results of the measurement of temperature coefficients using such plates. Furthermore, we informed that temperature coefficients of adiabatic elastic constants of c_{44} , c_{14} etc. would be calculated and that these results would be presented later. In this paper, we will discuss on this issue.

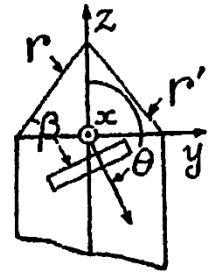


Figure 1

Variation of frequency f in equation (1) by temperature is given as

$$2 \frac{1}{f} \frac{\partial f}{\partial T} = \frac{1}{c} \frac{\partial c}{\partial T} - \frac{1}{\rho} \frac{\partial \rho}{\partial T} - 2 \frac{1}{a} \frac{\partial a}{\partial T} \quad \text{----- (2)}$$

Line expansion coefficients of line of length a with the arbitrary direction (direction cosine l , m , and n) having density ρ is given as

$$-\frac{1}{\rho} \frac{\partial \rho}{\partial T} = \frac{1}{x} \frac{\partial x}{\partial T} + \frac{1}{y} \frac{\partial y}{\partial T} + \frac{1}{z} \frac{\partial z}{\partial T} \quad \text{----- (3)}$$

$$\frac{1}{a} \frac{\partial a}{\partial T} = l^2 \frac{1}{x} \frac{\partial x}{\partial T} + m^2 \frac{1}{y} \frac{\partial y}{\partial T} + n^2 \frac{1}{z} \frac{\partial z}{\partial T} \quad \text{----- (4)}$$

$$\left. \begin{aligned} \frac{1}{x} \frac{\partial x}{\partial T} &= \frac{1}{y} \frac{\partial y}{\partial T} = 13.7 \times 10^{-6} / ^\circ\text{C} \\ \frac{1}{z} \frac{\partial z}{\partial T} &= 7.5 \times 10^{-6} / ^\circ\text{C} \end{aligned} \right\} \quad \text{----- (5)}$$

(by G. W. C. Kaye and T. H. Laby : "Physical and Chemical Constants", p.56)

Therefore, equation (2) of temperature coefficient becomes as

$$2 \frac{1}{f} \frac{\partial f}{\partial T} = \frac{1}{c} \frac{\partial c}{\partial T} + (7.5 + 12.4 \times \cos^2 \theta) \times 10^{-6} \quad \text{----- (6)}$$

By measuring frequencies and temperature coefficients for plates cut at $\theta = 140^\circ$ (angle between X-axis and the plate face was within 0.5°) and $\theta = 90^\circ$ (correspond to Y-cut and angle between X-axis and the plate face was within 0.5° .) are shown in Table 1 and Fig 2.

Temperature coefficients of Y-cut plate increase along with the decrease of the thickness of plates and reach the values listed in Table1.

From Fig 2, at $\beta = 9^\circ 46'$ ($\theta = 137^\circ 59'$) and $\theta = 54^\circ 45'$ (This angle was reported in the paper published on October, 1933) temperature coefficients become zero.

We substitute these values and temperature coefficient $103 \times 10^{-6}/^\circ\text{C}$ at $\theta = 90^\circ$ into equation (6) as follows,

Table 1

β	θ	dimension	freq.	Temperature coefficient
		mm ³	kc	$\times 10^{-6}/^\circ\text{C}$
-38° 13'	90° 00'	4.99 × 21.7 × 27.0	3 925.6	+103
-38° 13'	90° 00'	5.74 × 21.1 × 26.3	3 396.7	+103
-38° 13'	90° 00'	7.16 × 26.6 × 26.7	2 727.0	+103
8° 57'	137° 10'	5.41 × 25.8 × 29.6	4 661.9	+1.9
9° 31'	137° 44'	5.42 × 22.2 × 28.3	4 654.6	+0.6
9° 58'	138° 11'	4.95 × 25.9 × 30.1	5 088.5	-0.5
10° 34'	138° 47'	5.42 × 25.0 × 29.2	4 653.6	-1.9

Narrow side of the plate is in parallel with X-axis. Frequency measured at 21°C

$$0 = \left(\frac{1}{c} \frac{\partial c}{\partial T} \right)_{137^\circ 59'} + (7.5 + 12.4 \times \cos^2 137^\circ 59') \times 10^{-6} \dots\dots\dots (7)$$

$$0 = \left(\frac{1}{c} \frac{\partial c}{\partial T} \right)_{54^\circ 45'} + (7.5 + 12.4 \times \cos^2 54^\circ 45') \times 10^{-6} \dots\dots\dots (8)$$

$$2 \times 103 \times 10^{-6} = \left(\frac{1}{c} \frac{\partial c}{\partial T} \right)_{90^\circ} + 7.5 \times 10^{-6} \dots\dots\dots (9)$$

Then we use following values.

$$\left. \begin{aligned} c_{66} &= \frac{1}{2}(c_{11} - c_{12}) = \frac{1}{2}(85.45 - 7.26) \times 10^{10} \text{ dynes/cm}^2 \\ c_{44} &= 57.09 \times 10^{10} \text{ dynes/cm}^2 \\ c_{14} &= -16.87 \times 10^{10} \text{ dynes/cm}^2 \end{aligned} \right\} \dots\dots\dots (10)$$

From equations (9), (1) and (10),

$$\left. \begin{aligned} \left(\frac{1}{c} \frac{\partial c}{\partial T} \right)_{90^\circ} &= \frac{1}{c_{66}} \frac{\partial c_{66}}{\partial T} = +199 \times 10^{-6} \\ \frac{\partial c_{66}}{\partial T} &= +77.8 \times 10^6 \end{aligned} \right\} \dots\dots (11)$$

(+77.8X10⁶ in the original Japanese text is typo)

It is obvious that

$$\frac{\partial c}{\partial T} = \sin^2 \theta \frac{\partial c_{66}}{\partial T} + \cos^2 \theta \frac{\partial c_{44}}{\partial T} + \sin 2\theta \frac{\partial c_{14}}{\partial T} \dots (12)$$

From equations (7), (8), (10), (11) and (12)

$$\frac{\partial c_{44}}{\partial T} = -113.5 \times 10^6, \quad \frac{1}{c_{44}} \frac{\partial c_{44}}{\partial T} = -199 \times 10^{-6} \dots (13)$$

$$\frac{\partial c_{14}}{\partial T} = -18.5 \times 10^6, \quad \frac{1}{c_{14}} \frac{\partial c_{14}}{\partial T} = +110 \times 10^{-6} \dots\dots (14)$$

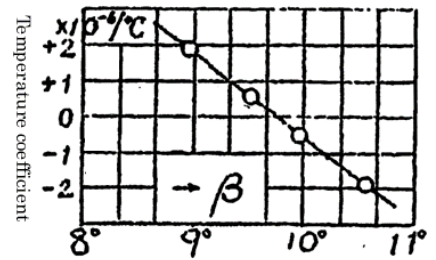


Figure 2

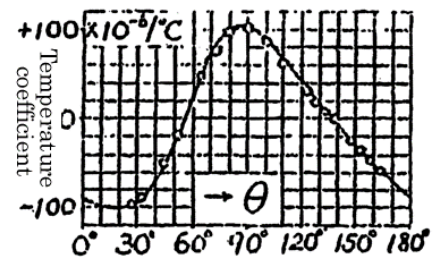


Figure 3

Once we obtain temperature coefficients of adiabatic eristic constants, we can derive temperature coefficients of frequency using equations (1), (6), (11), (13) and (14). Figure 3 indicate the results of the calculation. Several small circles around the curve in Figure 3 correspond to the measured values of temperature coefficients which we reported in the previous paper on October 1933. The curve in Figure 3 shows good agreement with the experimental data.

Additionally, Temperature coefficient C_{11} in equation $C_{60} = \frac{1}{2} (C_{11} - C_{12})$ can be calculated by measuring temperature coefficient of frequency of X-cut plate. Then we can get temperature coefficient of C_{12} . We will report these in the next time.

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