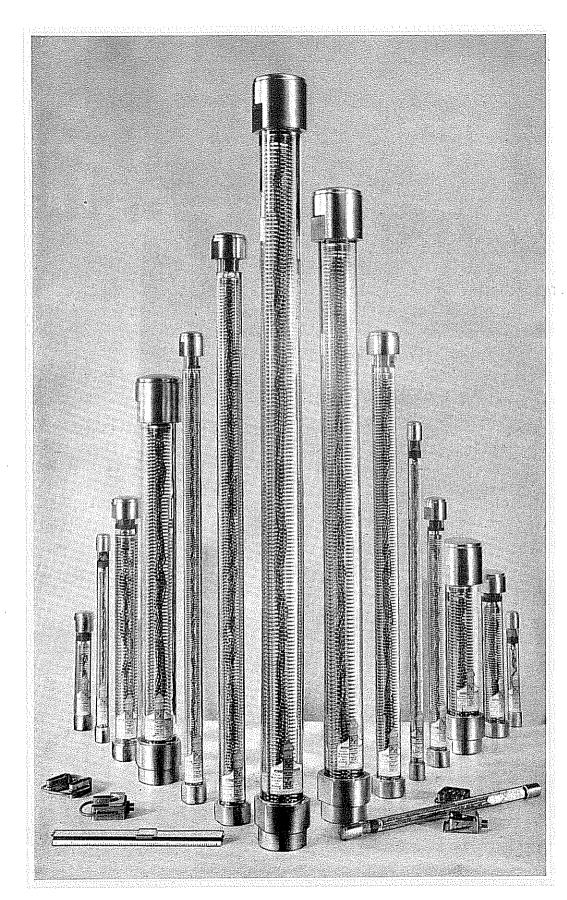


4435 RAVENSWOOD AVENUE

Chicago, Illinois, U. S. A.



2,200 to 138,000 Volts

½ to 400 Amperes

Trade Name and Patents

Although it is occasionally referred to and described in the trade as "Carbon Tetrachloride," "Tetrachloride," "Pyrene," "Liquid," and "Chemical" Fuse, the correct trade name is "S&C Fuse."

The manufacture, sale and use are controlled by United States and Foreign Patents, granted and pending. In the United States of America, the S&C Fuse is manufactured only by Schweitzer & Conrad, Inc., Chicago.

the LERIN 201-II

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Page 1

And Its Relation to Electric Power Systems

Electric Power Systems

The extension and inter-connection of electric power systems has contributed largely to national prosperity, by making available an economical source of energy for power, lighting, and heating purposes in practically all communities.

These inter-connections have effected considerable savings in generation and distribution costs through the advantages obtained from a diversity of loads, and by making possible the construction of large and efficient generating stations at locations where electric production costs are a minimum.

A Problem in Transmission and Distribution of Power

Continuity of service on transmission and distribution systems is, however, difficult to maintain, because the failure of a transformer causes a service interruption of the primary circuit to which it is connected, unless means are provided for the rapid and effective isolation of the defective transformer.

A transformer failure may result from an overload, short circuit, or abnormal voltage. The rapid and effective isolation of a defective transformer requires the application of protective equipment which will successfully interrupt abnormal current of values ranging from the minimum required to operate the protective device to the maximum short circuit current.

The Isolation of Defective Equipment

The automatic isolation of defective equipment is accomplished by either oil circuit breakers or fuses. Oil circuit breakers, on account of their high initial and maintenance costs, and the installation space requirements, are in numerous cases not justified. For this reason fuses, and particularly S&C Fuses, have found an ever increasing field of usefulness.

High Voltage Arcs

Interrupting a high voltage circuit under load is certain to be accompanied by an are which must be disposed of in some manner before it reaches destructive proportions.

A brief consideration of the characteristics of a high voltage are will show the fundamental features which high voltage circuit interrupting equipment must possess in order to clear the circuit during both overload and short circuit conditions.

Fig. 1 shows in graphic form the relation existing between the line voltage, the current, and the arc voltage, during the opening but before the final clearing of a high voltage non-inductive circuit.

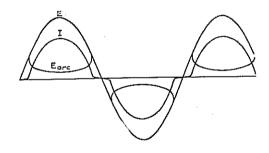


Fig. 1—Non-Inductive Circuit. E-Line Voltage; I-Current; E_{arc}-Arc Voltage

Immediately upon the opening of the circuit, a voltage appears across the gaseous gap (i. e. the arc voltage) which is in phase with the current. During the latter portion of each half cycle the arc becomes unstable and its resistance increases rapidly, causing the current to diminish to zero a small interval of time before the line voltage becomes zero. The arc is re-established during the following one-half cycle, as shown in Fig. 1, unless a gap has been established having a flash-over value greater than the highest instantaneous value of the line voltage.

And the Requirements for Interrupting High Voltage Circuits

Fig. 2 shows in graphic form the relation existing between the line voltage, the current, and the are voltage during the opening, but before the final clearing, of a high voltage

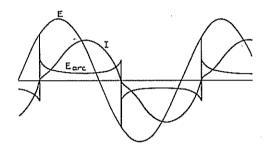


Fig. 2—Inductive Circuit—60° displacement between current and voltage. E-Line Voltage; I-Current; E_{arc}-Arc Voltage

inductive circuit. This graph shows that there is always a voltage available for the instantaneous re-establishment of the arc at the instant the current is zero. The voltage which causes the re-establishment of the arc increases with the inductance in the circuit, and becomes a maximum when a 90° phase displacement exists between the line voltage and the current. Inductance, therefore, greatly increases the difficulty of interrupting the circuit.

Fundamental Requirements for the Interruption of a High Voltage Circuit

From Figures 1 and 2 it is evident that a fundamental requirement for the successful interruption of a high voltage circuit is the introduction of a gap, the dielectric strength of which increases at a sufficient rate, follow-

ing current zero, to prevent the recovery voltage from re-establishing the arc. It will also be apparent that such a gap must be established in a minimum of time to prevent destruction of the circuit-interrupting equipment due to the thermal effect of the arc.

An arc in reality is a conductor, which automatically adjusts its cross section so as to maintain a constant current density. An arc may develop considerable physical proportions during a short circuit, and this necessitates some reliable means for rapidly extinguishing the arc. Immediately following the interruption of a short circuit in modern systems, the system voltage often reaches several times its normal value due to the sudden release of the stored energy of the system, which phenomenon increases the chances for the failure of the circuit-interrupting equipment.

Methods Employed for Interrupting High Voltage Circuits

Several methods for interrupting high voltage circuits have been applied by manufacturers. In expulsion fuses, for instance, sufficient vaporization of the fuse element and fuse tube liner must take place to expel conducting vapors and metals from the fuse tube. Others place the fuse element in a tube filled with powdered or granular materials and depend upon this material to absorb the vaporized fuse metal, and to extinguish the arc. In the case of an oil circuit breaker or an S&C Fuse, the gap is formed in the circuit by positive mechanical means, and the arc is extinguished by a liquid dielectric.

And the Fundamentals of High Voltage Fuse Design

Requirements for a Successful Fuse

During failure of equipment, the current may vary from over-current to short circuit of considerable magnitude. Also the phase relationship between the current and voltage, the point on the voltage wave at which the short circuit occurs during equipment failure, will be subject to wide variations. When these facts are considered together with the conditions outlined in foregoing paragraphs, it will be apparent that the fundamental requirements of a high voltage fuse are:

- (1) The fuse element should be of minimum section and length so as to reduce the quantity of ionized metal vapor to a minimum.
- (2) The fuse assembly must incorporate a positive means of lengthening and extinguishing the arc in the fuse tube, setting up a gap having a flashover voltage greater than the maximum transient value of the line voltage.
- (3) The fuse assembly must be self vented to prevent destructive pressures during short circuits.

Principles of the S & C Fuse

An examination of the illustration on the opposite page will show that the following features which are so necessary for the interruption of high voltage circuits, have been incorporated in the design of the S&C Fuse.

- (1) The fuse element is proportioned and assembled in a manner resulting in uniform time current characteristics and also in a minimum of ionized vapor when the fuse is blown.
- (2) A vent cap is provided for releasing the pressure when the fuse is blown during short circuit. The entire assembly is enclosed in a heat resisting glass tube which will withstand a hydraulic test pressure in the nature of 1000 lbs. per square inch.

- (3) A positive gap is introduced into the circuit by the rapid retraction of the moving arcing terminal through a liquid of high dielectric strength, this gap being formed by the action of the fuse spring, regardless of whether the fuse element is blown during overload or short circuit conditions.
- (4) The fuse element is shielded by the brass ferrule, completely protecting it from corona, which makes possible the manufacture of successful fuses for 2.2 Kv. to 138 Kv. having an ampere rating as low as one-half ampere.

Compared With an Oil Circuit Breaker

The operation of an S&C Fuse immediately following the melting of the fuse element is similar to the operation of an oil circuit breaker, but in addition the former has the following advantages:

- (1) The arc is quenched in a non-inflammable liquid of high dielectric strength. The vapors of this liquid will not support combustion.
- (2) The moving areing terminal of an S&C Fuse possesses practically no inertia, and as a result of the speed of the terminal the fuse clears short circuits in ½ to 2 cycles after the fuse element has melted, whereas, an oil circuit breaker will require from 8 to 60 cycles to clear the circuit, after the trip coil has been energized.
- (3) When an S&C Fuse is blown under short circuit, the replacing of the fuse completes the necessary maintenance, whereas, under similar conditions an oil circuit breaker would require inspection of contacts, and filtering and drying of oil to restore it to its original condition; thus resulting in a maintenance expense many times greater than the refill cost of a set of S&C Fuses.

How the S&C Fuse Operates

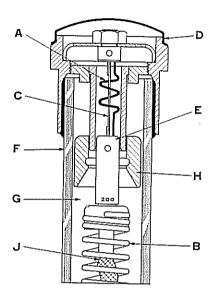


Fig. 3

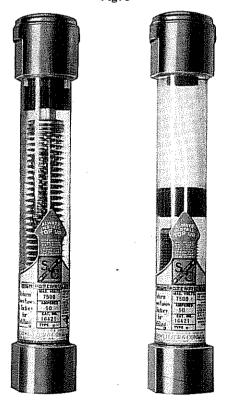


Fig. 4 Fig. 4A
Normal S&C Fuse—and after blowing

The Principal Parts

A typical S&C Type D Fuse as shown, in three views at the left, consists essentially of:

- A—Fuse Element—designed to melt at definite current values.
- B—Coil Spring—normally extended.
- C—Strain Wire of high resistance and high tensile strength — holding the coil spring extended.
- D—Vent Cap—for relieving excessive pressure.
- E—Moving Terminals—acts as areing terminal when the fuse blows.
- F—Heavy heat resisting Glass Tube—sealed into brass ferrules.
- G—Arc-extinguishing Liquid—filling glass tube.
- H—Funnel-Shaped Liquid Director or Nozzle—attached to areing terminal.
- J—Flexible Copper Cable—for carrying the current and thus preventing heating of the spring.

Fuse Operation

In a circuit protected by the S&C Fuse, when the current reaches a certain predetermined value, the fuse element (A) melts, shunting the load current to the strain wire (C) and this wire, being of small current carrying capacity, instantly melts and allows the coil spring (B) to contract.

The contracting of the fuse spring, accelerated by the volatilization of the fuse element during heavy short circuits, forces a stream of liquid into the confined areing zone where it is rapidly volatilized, developing pressures which force the vapor through the arc stream. This action results in the rapid de-ionization, or in other words, the quick recovery of the dielectric strength of the space occupied by the arc as the current approaches zero. This process is very rapid, and complete extinction of the arc is accomplished in ½ to 2 cycles.

In most cases the fuse simply functions in the manner described above. In cases of severe operation, such as short circuit on a system of large capacity, the pressure in the fuse tube is released through the safety vent cap (D) provided for that purpose.

Two Types of Construction of the S&C Fuse

Two types of fuse construction, designated as "B" and "D" are manufactured to cover the range of 2,200 to 138,000 volts and $\frac{1}{2}$ to 400 amperes, as listed on pages 14 and 15.

Fuses of type B construction are supplied in the lower current ratings and up to 69,000 volts. Fuses of the type D construction have extra high interrupting capacity and are always supplied in the higher current ratings up to 69,000 volts and all current ratings at higher voltages. Type D Fuses are available also for lower current ratings at the lower voltages in order to provide the extra high interrupting capacity sometimes desirable for those ratings. (See table of interrupting capacities, page 12-A.)

Type B Fuse Construction

The drawing at the right shows the Type B construction of the S&C Fuse. In this type, the fuse element is enclosed in an arc barrier of insulating material.

Type B Fuse Clips

In the Type B construction the ferrules of the fuse are cylindrical and the Type B Clips have a corresponding circular form where they grip the ferrules. A Type B Clip is illustrated at the right. It is to be noted that the fuse is held under spring pressure from the clip, and this is augmented by pressure from the retaining bale which exerts a squeezing effect upon the clip as the bale is swung into place over, and locked by, a projecting boss.

Not only do the S&C Fuse Clips provide ample contact, but in addition they hold the fuse with more than usual firmness. As a result, the contact surfaces are not easily corroded and the fuse will not be thrown out of the clips when it is subjected to the powerful magnetic forces resulting from a short circuit.

The S&C Fuse Clips just described are always included on fuse mountings regularly supplied by Schweitzer & Conrad, Inc. When fuse mountings are purchased elsewhere, the genuine S&C Fuse Clips should be specified for use with S&C Fuses.

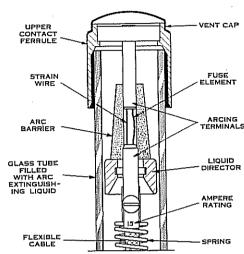


Fig. 5—Upper Portion of Type B S & C Fuse showing principal parts.

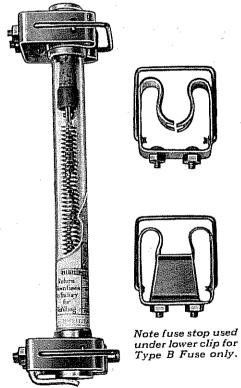


Fig. 6—Type B, S & C Fuse as supported in clips. Also bottom view of clips separately.

Two Types of Construction of the S&C Fuse—Cont'd.

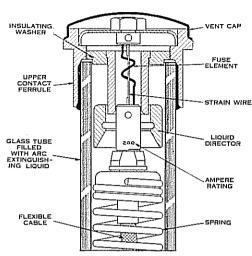


Fig. 7—Upper Portion of Type D, S&C Fuse Showing Principal Parts

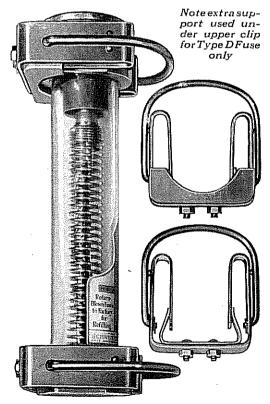


Fig. 8—Type D, S&C Fuse as Supported in Clips. Also Bottom View of Clips Separately

Type D Construction

In the Type D Construction, the fuse element is placed in a separate "explosion chamber" at the upper end of the fuse and above the level of the liquid.

When a Type D Fuse is blown during overload or short circuit, the pressure resulting from vaporization of the Fuse Element is confined to the chamber above the Arcing Terminal and below the Vent Cap. The result is that during short circuit the vent cap blows off before excessive pressures develop in the glass tube.

Type D Fuse Clips

In the Type D Fuse Construction the ferrules have flat contact surfaces. The ferrules of the Type D Fuse are larger than the Type B and the flat contact surfaces allow easy insertion and removal of the fuse regardless of the heavy pressure from the double spring action of the clips.

Like the Type B Clips described on the opposite page, the Type D Clips hold the fuse firmly under all conditions by means of the retaining baits and provide contact which is not likely to be impaired by corrosion. For that reason users of the S&C Fuse should specify the genuine S&C Fuse Clips if mountings are ordered from other manufacturers.

Type DLC (Low Current) Fuse

The Type DLC is a variation of the Type D Construction in which a very low current rating is combined with high interrupting capacity. This assembly consists of an ingenious combination of levers and fuse element arranged so that only a small fraction of the tension of the heavy spring is transmitted to the small fuse element.

The application of this assembly makes possible a current rating as low as ½ ampere, with an over-all mechanical strength equal to that of S&C fuses of the higher ampere ratings. This fuse element is sufficiently large to withstand the initial rush of current occurring during the energizing of the transformer, will earry the load current continuously, and will be blown by the current which flows through the primary winding of a standard potential transformer during a short circuit at or near the secondary terminals.

Has Seven Important Advantages

1. Reliable Time-Current Characteristics

The time-current characteristics of the S&C Fuse are reliable because each fuse is made the same as every other one of its kind by precision methods which bring about strict uniformity.

2. Dependable Operation

Its current-interrupting ability at low or high short-circuit currents is the result of good design. Its dependability is the result of meticulous care in manufacturing, wherein each fuse is given seven different tests during the process.

3. Rapid Clearing Time

The clearing time of the S&C Fuse is equally rapid whether the fuse element is blown on overload or short circuit.

4. Does Not Hazard Adjacent Equipment

There is no expulsion of long pieces of conducting materials such as the unvaporized portion of the fuse element or cable.

5. Venting Is Upward

When an S&C Fuse is blown during short circuit the internal pressure is relieved at the top which means that it is in a direction away from an operator.

Factory Refill Restores Original Interrupting Capacity

The fact that an S&C Fuse must be refilled at the factory with special equipment results in the assurance that a subsequent operation of a fuse will not be hampered by an injury which might have occurred in a previous operation and go unnoticed by the repairman. (See also next column.)

7. Blown Fuse Distinguishable at a Distance

The S&C Fuse when blown is distinguishable at a distance (see Fig. 10.) This saves both time and expense.

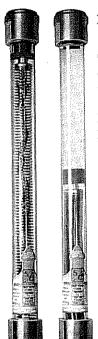


Fig. 9

Liquid Will Not Freeze

The liquid used in the S&C Fuse will not freeze in any elimate in which it might be used.

Return Blown Fuses to the Factory for Refilling

Blown fuses returned to the factory for refilling are first disassembled; all obsolete or damaged parts are discarded and the remaining parts which meet the mechanical and electrical requirements are thoroughly cleaned. The fuses are then re-assembled, just as new fuses are assembled, and the latest improvements are always incorporated. Thus when S&C Fuses are refilled

they are made the same as new fuses of the current design.

This refilling, which is actually reconstructing, therefore, wipes out all depreciation or obsolescence which might be charged against fuses regardless of when they were originally purchased.

Although extreme care and special processes requiring special equipment are necessary to do the work properly, the cost of refilling is not high. When it is understood that the refill charge covers complete rejuvenation of the fuses, and therefore disposes of depreciation and obsolescence, the charge is found to be remarkably low.

Special Field Tests Have Shown Definitely Satisfactory Results

For a number of years S&C Fuses have been applied by electric service companies in installations connected to their distribution and transmission systems where very high grade circuit-interrupting equipment is required. This extended service experience has developed a well earned reputation for the S&C Fuse as being capable and dependable under severe operating conditions.

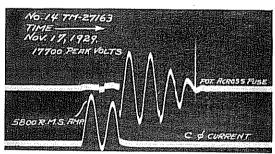


Fig. 11—S&C, 25 kv., 1 ampere, Size 3, Fuse clearing 5800 rms amperes

Numerous tests were made to determine the performance of new designs before placing them on the market. Also many tests have been made by power companies to verify the interrupting capacity. Such tests have been made under a variety of conditions and have shown the ability of this fuse to

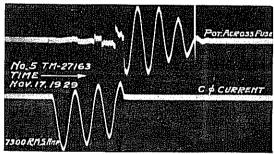


Fig. 12—S&C, 25 kv., 400 ampere, Size 5, Fuse clearing 7300 rms amperes

interrupt currents, from the smallest amount necessary to melt the fuse element, to enormous short circuits, with a certainty and rapidity not always attributed to this class of equipment.

The oscillogram records shown here were made during tests on large metropolitan systems. They are typical of the records of

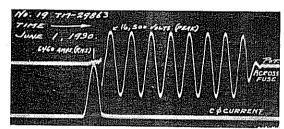


Fig. 13—S&C, 25 kv., 100 ampere, Size 4, Fuse clearing 6460 rms amperes

a large number of tests at each of the voltages shown and represent in a fair way the performance of the S&C Fuse on these occasions.

The oscillograms shown in Figures 11, 12 and 13 were obtained by short circuiting one phase of a 12 kv., 60 cycle system thru an S&C Fuse. From the standpoint of voltage across the fuses, these tests were the equivalent

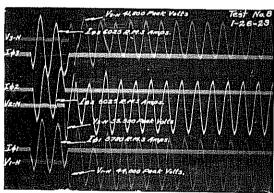


Fig. 14—S&C, 50 kv., 75 ampere, Size 4, Fuses clearing a 3-phase short circuit on a 44 kv. system

of a 22 kv., 3-phase short circuit to neutral or a 22 kv., 1-phase short circuit involving two fuses. These tests were unusually severe, because the high inductance in the test circuit resulted in approximately a 90° phase displacement between current and voltage.

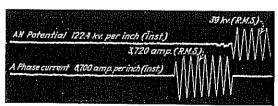


Fig. 15—S&C, Size 5, Fuse clearing a phase to neutral short circuit on a 66 kv. system

S&C Fuse Application Recommendations

For Power and Distribution Application

The proper application of high voltage fuses in power and distribution transformer installations requires that consideration be given to both the transient and normal load conditions which may occur during operation. Detailed investigation of transient conditions shows that:

- (1) The energizing of an unloaded transformer is often accompanied by an initial rush of current several times the full-load current rating of the transformer, whereas the exciting current, a few cycles after energizing the transformer, is only from 3 to 5% of the full-load current rating.
- (2) The energizing of an incandescent lamp load is accompanied by a rush of current approximately five times normal, because of the high positive temperature coefficient of the tungsten filament. This rush of current decreases rapidly due to the increase in the lamp filament resistance with increasing temperature, and becomes normal in a few cycles.
- (3) The starting current drawn by squirrel cage motors amounts to from 250 to 400% of the full-load current rating of the motors.

No damage results from such momentary overcurrents, providing that they do not persist until destructive temperatures have developed in the transformer windings.

In the case of large transformers, the momentary over-capacity demands will generally be a smaller percentage of the transformer rating than in the case of small transformers, because large transformers supply a number of different loads, the transient current demands of which do not occur at the same instant.

After taking these facts into consideration it will be apparent that to prevent unnecessary interruptions to service, due to transient conditions, the high tension fuse must be selected by referring to its time-current characteristics, and in general its ampere rating must be several times the full load current rating of the transformer.

An attempt should not be made to apply high tension fuses to protect a transformer during overloads of 150 to 200 per cent of the transformer full-load current rating, because unnecessary fuse operation will result during transient conditions which do not last a sufficient length of time to develop destructive temperatures in the transformer windings. Where overload protection is considered necessary, it should be obtained by the installation of fuses or circuit breakers on the secondary side of the transformers.

The most satisfactory results will be obtained when S & C Fuses are applied for isolating the transformers, and for protecting the system during extreme overload or short circuits resulting from grounds or breakdown of equipment.

Table of Recommendations

The table, page 12, gives recommendations for the application of S & C Fuses in distribution and power transformer installations for the purpose of isolating the transformer from the system during short circuits or insulation failures.

Ampere Rating of S & C Fuse to Use

When a fuse is desired for carrying the normal and transient current in a transformer installation, the required ampere rating can

S & C Fuse Application Recommendations—Cont'd

be determined from the tabulation shown on page 12. Application of fuses according to this tabulation will result in very prompt isolation of the transformer in case of insulation failure. This tabulation, however, does not take into account the time delay which may be required in the high tension fuse for a particular installation.

When selective action is desired between secondary circuit-interrupting equipment and the high tension fuse, the ampere rating of the S & C Fuse can be determined readily by reference to the alignment chart on page 12B.

Interrupting Capacity

After selecting the ampere rating of the fuse required, the fuse tube size should be selected so as to obtain sufficient interrupting capacity to clear the maximum short circuit which can occur in the case of a failure at the primary terminals of the transformer. A table of interrupting capacities for the various tube sizes and voltages of S & C Fuses is shown on page 12A.

Voltage Rating

The voltage rating of the fuse should always be at least equal to the system voltage.

The voltage ratings given on S & C Fuses are in accordance with the recently adopted standard voltage ratings for general apparatus.

Number of Fuses to Use

Two fuses should always be installed in a single-phase installation and three fuses should always be installed in a three-phase installation.

For Potential Transformer Application

Either the Type B—"PT," or the Type DLC, S & C Fuse should be applied in potential transformer installations.

The Type B—"PT" is suitable for disconnecting the transformer in case of transformer failure.

The Type DLC ½ ampere fuse will disconnect a potential transformer during a short circuit at the secondary terminals, as well as during a transformer failure.

For 2300 to 33,000 volt potential transformer installations, the $\frac{1}{2}$ ampere, Type

DLC Fuse is recommended. In higher voltage installations, or where the capacity of the transformer is in excess of 200 voltamperes, the 1 ampere, Type DLC Fuse should be applied.

When the possible short circuit current which will flow during a potential transformer failure exceeds the interrupting capacity of the potential transformer fuse, the S & C Wire Wound Resistor should be applied in connection with the S & C, Type DLC Fuse.

A bulletin describing S & C Current-Limiting Resistors and their application is available and will be furnished upon request.

Other Applications

The numerous applications of S & C Fuses not coming under the foregoing classes are best treated by individual recommendations. Among such applications are the following:

- 1. To disconnect carrier current coupling condensers in case of condenser failure.
- 2. To disconnect telephone equipment when telephone lines come in contact with power lines.
- 3. For the purpose of shunting distribution feeder reactors during normal operation so as to improve the circuit voltage regulation and reduce the loss. During a short circuit the fuse blows, cutting the reactors into service before the oil circuit breakers have time to open.
- 4. To prevent line interruptions due to suspension insulator flashovers during lightning disturbances.
- 5. To prevent service interruptions due to lightning arrester failure.
- 6. To prevent service interruption due to static condenser failure.
- 7. On high voltage D.C. electric railway circuits.
- 8. In radio broadcasting for interrupting the high voltage, highly inductive plate circuit during tube failure.

Table of Recommendations for Application of the S&C Fuse

Recommended fuse ratings for SINGLE-PHASE transformer installations at various system voltages

1-Ph.	2,300	Volts	4,000	Volts	6,600	Volts	11,000	Volts	13,200	Volts	22,000	Volts	33,000	Volts	1-Ph.
K V A	Full Load Amp,	Rating of Fuse Amp.	Full Load Amp.	Rating of Fuse Amp.	Full Load Amp.	Rating of Fuse Amp.	Full Load Amp.	Rating of Fuse Amp.	Full Load Amp.	Rating of Fuse Amp.	Full Load Amp.	Rating of Fuse Amp.	Full Load Amp.	Rating of Fuse Amp.	K V A
1.5 2.5 3 5	$0.65 \\ 1.09 \\ 1.30 \\ 2.18$		0.38 0.63 0.75 1.25	3 3	0.23 0.38 0.46 0.76	2 2 2 3	0.23 0.27 0.46	2 2 2	0.19 0.23 0.38		0.23	2			$egin{array}{c} 1.5 \ 2.5 \ 3 \ 5 \end{array}$
7.5 10 15 25	$ \begin{array}{r} 3.26 \\ 4.35 \\ 6.53 \\ 10.9 \end{array} $		1.87 2.50 3.75 6.25	8	$ \begin{array}{r} 1.14 \\ 1.52 \\ 2.27 \\ 3.79 \end{array} $	5 5 8 12	0.68 0.91 1.37 2.27	3 3 5 8	0.57 0.76 1.14 1.89	3 3 5 S	$\begin{array}{r} 0.34 \\ 0.46 \\ 0.68 \\ 1.14 \end{array}$	3	0.30 0.46 0.76	2	7.5 10 15 25
37.5 50 75 100	16.3 21.8 32.6 43.5	40 50 75 100	9.37 12.5 18.7 25.0	25 30 40 50	5.68 7.58 11.4 15.2	15	3.41 4.55 6.82 9.10	10 12 20 25	2.84 3.79 5.68 7.58	10 12 15 20	1.70 2.27 3.41 4.55	5 8 10	1.14 1.52 2.27 3.03	5 5 8 10	37.5 50 75 100
150 200 250 333	65.3 87.0 109 145	200 200 250 300	37.5 50.0 62.5 83.1	75 100 200 200	22.7 30.3 37.9 50.5	50 60 100 100	13.7 18.2 22.7 30.3	30 40 50 60	11.4 15.2 18.9 25.2	30 40 40 50	$ \begin{array}{r} 6.82 \\ 9.10 \\ -11.4 \\ 15.2 \\ \hline \end{array} $	30 40	4.55 6.06 7.58 10.1	15 20 25	150 200 250 333
400	174	400	100	200	60.6	200	36.4	75	30.3	60	18.2	40	12.1	30	400

Recommended fuse ratings for THREE-PHASE transformer installations at various system voltages

3-Ph.	2,300 V	olts.	4,000 V	olts	6,600 \	olts	11,000	Volts	13,200	Volts	22,000	Volts	33,000	Volts	44,000	Volta	66,000	Volts	3-Ph.
K V A	Full Load Amp.	Hating of Fase Amp.		ilating of Fuse Amp.		Rating of Fuse Amp.	Full Load Amp.	Rating of Fuse Amp.	Full Load Amp.	Rating of Fuse Amp.	Full Load Ann.	Rating of Fuse Amp.	Full Load Amp.	Rating of Fuse Amp.		Rating of Puse Amp.	Full Lond Amp,	Rating of Fuse Amp.	K V A
4.5 5 7.5	1.13 1.25 1.88	5580	0.65 0.72 1.09 1.30	3 3 5 5	0.39 - 0.44 - 0.66 - 0.79	ବା ଦୀ ସ୍ଥର ସ	$0.39 \\ 0.47$	2 2	0.33 0.39	2 2									4.5 5 7.5 9
9 10 15 22.5	$\begin{array}{r} 2.26 \\ 2.50 \\ 3.77 \\ 5.65 \end{array}$	$-\frac{8}{8}$ 12 15	1.45 2.18 3.27	5 8 10	0.88 1.31 1.97	3555	0,53 0,79 1,18	2 3 5	0.44 0.66 0.99	2 3 3	0.39 0.59								10 15 22.5 25
25 30 37.5 45	$\begin{array}{r} 6.30 \\ \hline 7.54 \\ 9.43 \\ 11.3 \end{array}$	$ \begin{array}{r} 15 \\ \hline 20 \\ 25 \\ 30 \end{array} $	$ \begin{array}{r} 3.64 \\ 4.33 \\ 5.42 \\ 6.50 \end{array} $	$\frac{12}{12}$ $\frac{15}{15}$	$\begin{array}{r} 2.19 \\ \hline 2.63 \\ 3.28 \\ 3.94 \end{array}$	$\frac{8}{8}$ 10 12	$\begin{array}{r} 1.31 \\ \hline 1.58 \\ 1.97 \\ 2.36 \end{array}$	5 8 8	$\begin{array}{r} 1.09 \\ \hline 1.31 \\ 1.64 \\ 1.97 \end{array}$	5 5 8	0.66 0.79 0.99 1.18	3 3 5	0.53 0.66 0.79	3	0.59	3			30 37.5 45
50 75 100 112.5	12.6 18.8 25.1 28.3	30 40 50 60	$ \begin{array}{r} 7.24 \\ \hline 10.9 \\ 14.5 \\ 16.3 \end{array} $	$ \begin{array}{r} 20 \\ \hline 25 \\ 40 \\ 40 \end{array} $	$ \begin{array}{r} 4.38 \\ \hline 6.58 \\ 8.70 \\ 9.85 \end{array} $		$ \begin{array}{r} 2.63 \\ \hline 3.94 \\ \hline 5.27 \\ \hline 5.92 \\ \end{array} $	12 15 15	$ \begin{array}{r} 2.19 \\ \hline 3.28 \\ 4.38 \\ \hline 4.93 \\ \end{array} $	10 12 15	$\begin{array}{r} 1.31 \\ \hline 1.97 \\ 2.63 \\ 2.96 \end{array}$	8	$\begin{array}{r} 0.88 \\ \hline 1.31 \\ 1.75 \\ 1.97 \end{array}$	5 5 8	0.66 0.99 1.31 1.48	3 5 5			50 75 100 112.5
150 200 225 300	37.7 50.3 50.5 75.4	75 100 150 150	$ \begin{array}{r} 21.8 \\ \hline 28.9 \\ 32.7 \\ 43.3 \end{array} $	50 60 75 100	13.1 17.5 19.7 26.3	30 40 40 60	7.90 10.5 11.8 15.8	20 25 30 40	6.58 8.76 9.85 13.1	$ \begin{array}{r r} & 20 \\ \hline & 25 \\ & 25 \\ & 30 \\ \end{array} $	$ \begin{array}{r} 3.94 \\ \hline 5.27 \\ 5.92 \\ \hline 7.90 \\ \end{array} $	15 15	$\begin{array}{r} 2.63 \\ 3.50 \\ 3.94 \\ 5.27 \end{array}$	10 12 15	$\begin{array}{r} 1.97 \\ \hline 2.63 \\ 2.96 \\ 3.94 \end{array}$	$\frac{-8}{8}$ $\frac{10}{12}$	$\begin{array}{r} 1.31 \\ \hline 1.75 \\ 1.97 \\ 2.63 \end{array}$	8 8	200 225 300
450 600 750	113 151 188	$\frac{250}{300}$	65.0 86.7 109	200 200 250	39.4 52.7 65.8 87.6	100 100 200 200	$\begin{array}{ c c c }\hline 23.6\\\hline 31.6\\39.4\\52.7\\\hline\end{array}$	50 60 100 100	19.7 26.3 32.8 43.8	40 60 75 100	$\begin{array}{r} 11.8 \\ \hline 15.8 \\ 19.7 \\ 26.3 \end{array}$	30 40 40 60	$\begin{array}{r} 7.90 \\ \hline 10.5 \\ 13.1 \\ 17.5 \end{array}$	20 25 30 40	7.90 7.90 9.85 13.1	20 25 30	3.94 5.27 6.58 8.76	15 · 20	450 600 750 1,000
1,000 1,200 1,500 2,000			145 173	300 400	105 131 175	250 250 300 400	63.2 - 79.0 105	200 200 250	52.7 65.8 87.6	100 200 200	$\begin{array}{r} 31.6 \\ \hline 39.4 \\ 52.7 \end{array}$	100 100	21.2 26.3 35.0	50 60 75	15.8 19.7 26.3	40 40 60 75	10.5 13.1 17.5 21.9	25 30 40 50	1,200 1,500 2,000 2,500
2,500 3,000 3,750 5,000							$\frac{131}{158}$ $\overline{197}$		109 131 164	250 300 400	98.5 131	200 200 200 300	43.8 52.7 65.8 87.6	100 100 200 200	32.8 39.4 49.3 65.8	100 100 200	26.3 32.8. 43.8	$\frac{60}{75}$	3,000 3,750 5,000
6,000 7,500 10,000											158 197	400 400	105 131 175	$ \begin{array}{r r} 250 \\ 300 \\ \hline 400 \end{array} $	79.0 98.5 131	200 200 300	52.7 65.8 87.6	100 200 200	6,000 7,500 10,000

Higher Voltage Recommendations will be given on application.

Time-Current Curves and Data applicable to S & C Fuses will be furnished on request.

Application of S&C Fuses

In Locations Where Blowing Time Is of Particular Importance

The following statements pertain to installations containing S&C Fuses and also other types of circuit-interrupting equipment, such as circuit breakers or fuses. In such installations it is usually required that the circuit interrupting devices function selectively during equipment or line failures.

For instance, selective action may be required between-

- (a) Two fuses in the same circuit.
- (b) A circuit breaker and a fuse in the same circuit.
- (c) A low tension breaker and a high tension fuse.
- (d) A low tension fuse and a high tension fuse.

In order to make a proper selection of S&C Fuses for such installations, the following factors must be considered—

(1) Normal Full Load Current Through the Fuse.

The normal load current in a transformer installation should be considered as the current flowing when the transormer is loaded to rated capacity.

The normal load current of a circuit should be considered as the maximum current which the circuit may be called upon to carry.

The ampere rating of the S&C Fuse should not be less than 154% of the normal load current.

(2) Possible Short-Circuit Current.

The possible short-circuit current should be calculated by the conventional methods.

Where fuses are applied on the high tension side of a transformer or transformer bank, it is usually permissible to neglect the impedance external to the transformer when calculating the possible primary current during a secondary short.

(3) Opening and Clearing Time.

The blowing time of an S&C Fuse or any other make of fuse for any value of short-circuit current can be determined by reference to the time-current curves issued by the fuse manufacturer. The clearing time of a fuse during short circuit can be approximated by adding from one to two cycles to the blowing time.

In the case of a circuit breaker the clearing time can be approximated by adding one quarter of a second to the time required for the relay to close the circuit of the circuit breaker trip coil.

(4) Required Margin in Time to Insure the Desired Selective Action.

To prevent the temperature of an S&C Fuse element rising to a value dangerously close to the melting point, during the time taken by some other device to interrupt the fault current, the blowing time of the S&C Fuse for this current should be approximately 50% greater than the maximum clear-

ing time of the other device.

This margin of time will insure the desired selective action in all cases including those in which the fuse element will be subjected to the accumulation of heat during the operating cycles of an automatic reclosing breaker.

(5) Maximum Short-Circuit Current Which the Fuse May Be Called Upon to Interrupt.

This current will determine the fuse tube size which will be necessary to provide sufficient interrupting capacity.

A tabulation giving the interrupting capacities of the various sizes of S&C Fuses is to be found on this page.

The Alignment Chart on the following page will facilitate the selection of the proper ampere rating of the TYPE D S&C FUSES* to give the desired blowing time at any predetermined short-circuit current value. The straight edge of a rule placed across the 3 scales (I_s), (I_r) and (t) will give the corresponding values of these three factors.

The scales (Z) and (Ir), have been included to allow the short-circuit current to be determined in the same simple manner, when fuses are to be selected for transformer installations, and when the rated full load current and the percent impedance of the transformer are known. It will be found that in the majority of cases this method of determining the ampere rating of the fuse to use will be sufficiently accurate, if the margin of time recommended in paragraph (3) is adhered to, although this method neglects the impedance of the circuit external to the transformer.

The two dotted lines appearing in the chart illustrate the solution of the example

diagrammed at the right, in which

Z=5% $I_T=13.1$ amperes $t=1.5\times0.6=0.9$ seconds $I_T=?$

The line projected thru 5 on scale (Z) and 13.1 on scale (I_r) to scale (I_s),

shows that the primary current during a secondary short amounts to 262 amperes. The line connecting 262 amperes on scale (Is) and 0.9 seconds on scale (t), shows that the ampere rating of the fuse to use, I_F=75 amperes.

The smallest 75 ampere, S&C Fuse manufactured is supplied in the size 4 tube. The tabulation at the bottom of this page shows that a 34,500 volt, 75 ampere, size 4 fuse has an interrupting capacity of 5500 amperes. If the maximum short-circuit current in case of an insulation failure at the primary terminals of the transformer exceeds this value but does not exceed 6400 amperes, the application of a 34,500 volt, 75 ampere, size 5 fuse will provide the required interrupting capacity.

If Type B, S&C Fuses are to be applied in installations where selective action is required, the blowing time as a function of short-circuit current may be determined from the time-current curves of the Type B Fuses, which will gladly be furnished upon request.

*The scales (Ir), (Is) and (t) represent that portion of S&C time-current curve No. 111, which is of most interest in this connection. Time-current curve No. 111 pertains only to S&C 10 to 400 ampere, Type D, sizes 3 and 4 Fuses, as manufactured beginning July 25, 1930, and to Type D, size 5 Fuses, as manufactured beginning August 11, 1930. The date of man ufacture of any S&C Fusc is always stamped on the rule of the fuse

SEC FUSE

2300 VOLTS

CLEARING TIME

0.6 SEC

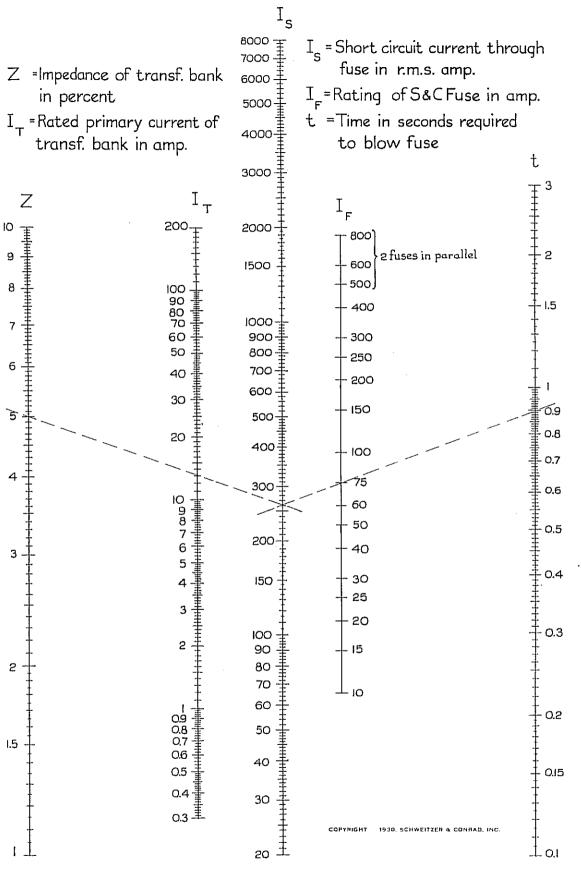
750 KVA 7000 33000 VOLT5

Interrupting Capacity of S&C Fuses in r.m.s. Amperes at 60 Cycles

	Voltage Rating & C Fuse	7500	23000	23000	34500	46000	69000
	System Voltage	4000	13200	22000	33000	4.1000	66000
Tube	1 and 2	Amp. 4500	Amp. 3900	А тр. 3300	Атр. 2750	Атр. 2200	Amp. 1500
Гияе	3	6900	5900	5100	4300	3700	2700
JO	-1	8600	7400	6500	5500	4600	3300
Size	5	10000	8700	7600	6400	5500	4000

For listing of available ampere ratings in various tube sizes for 7.5 to 138 kv., refer to pages 14 and 15.

Page 12-A



ALIGNMENT CHART

giving corresponding values of

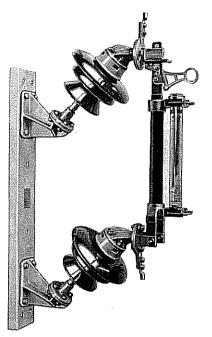
Short-Circuit Current, Blowing Time and Ampere Rating of 10 to 400 amp. Type D S&C Fuses (time-current curve No. 111)

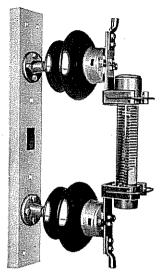
The S&C Fuse

Should Be Installed with Top Up

The S&C Fuse is designed for installation in a vertical position with the vent cap up (see Fig. 3, page 5), in which position the blowing of the fuse element is followed by the maximum speed of the arcing terminal, and the maximum benefit is derived from the

voltage may rise to several times its normal value due to the sudden release of stored energy. S&C engineers realize the importance of taking this fact into consideration and have designed all S&C Fuse Mountings with a proper regard for normal and possible abnormal voltage stresses.





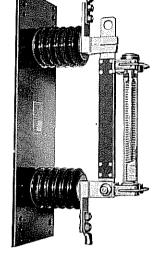


Fig. 17—25,000-Volt Type B-M Outdoor Fuse Mounting

Fig. 18—15,000-Volt Type KC-SM Indoor Fused Disconnect

Fig. 16—37,000-Volt Type GK-SM Outdoor Fused Disconnect

arc-extinguishing liquid. When it is necessary to install the S&C Fuse at an angle, the angle should never be greater than 45° from the vertical, and the pressure vent should always be up.

A few typical S&C Mountings shown here, illustrate correct methods of fuse support.

Broad experience on fusing problems, working in conjunction with electric utility engineers, has given S&C engineers a thorough understanding of the necessity for extrastrength, in certain parts of fuse mountings, not ordinarily appreciated. S&C Fuse Mountings, therefore, embody the essential rigidity throughout and have the required gripping strength in the contact clips to enable S&C Fuses to operate unhampered by the mechanical deficiencies of incorrectly designed mountings.

Immediately following the interrupting of a short circuit, in a modern system, the

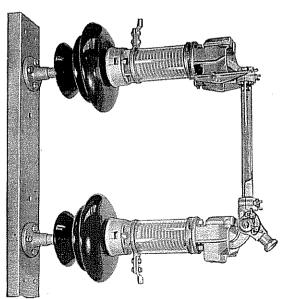


Fig. 19—37,000-Volt Type BJ-MRR-O "Pole-Pull" Fuse Mounting described on Page 18

The S&C Fuse

Ordering Information-7,500 to 46,000 Volts

		Maxin for Vo	00 Volts ium Rat Ituges uj	ing o to	Rate for 7.5	00 Volts d Voltag 01 to 23,	ge		500 Volts ed Voltag		16.0 Rate	100 Volts d Voltag	; 20		
Туре ‡	*Rating Am-	7.5	00 Volts Centers 8	- 1	Clip C	Volts enters 11	1 6"	Clip	Centers 1	5"	Clip	Centers 1	8"	*Rating Am- peres	Typa ‡
,	peres	Catalog Number	List Price	Tube Size	Catalog Number	List Price	Tube Size	Catalog Number	List Price	Tube Size	Cutalog Number	List Price	Tube Size		
***************************************	P. T.† 1 2 3	16001 16101 16111 16121	\$ 3.50 3.50 3.50 3.50	1 1 1	16003 16103 16113 16123	\$ 4.50 4.50 4.50 4.50	1 1 1	$\begin{array}{c} 16004 \\ 16104 \\ 16114 \\ 16124 \end{array}$	\$ 7.50 7.50 7.50 7.50	1 1 1	$\begin{array}{c} 16005 \\ 16105 \\ 16115 \\ 16125 \end{array}$	$\begin{array}{c} \$12.00 \\ 12.00 \\ 12.00 \\ 12.00 \\ 12.00 \end{array}$	1 1 1	P. T.† 1 2 3	_
Type B	5 8 10 12	$ \begin{array}{r} 16121 \\ \hline 16131 \\ 16141 \\ 16151 \\ 16201 \end{array} $	3.50 4.00 4.00 5.00	1 1 1 2	16133 16143 16153 16203	4.50 5.50 5.50 8.00	1 1 1 2	16134 16144 16154 16204	7.50 9.50 9.50 18.00	1 1 1 2	$\begin{array}{r} 16135 \\ 16145 \\ 16155 \\ 16205 \end{array}$	$\begin{array}{c} 12.00 \\ 15.00 \\ 15.00 \\ 28.00 \end{array}$		5 8 10 12	Type B
	15 20 25	16201 16211 16221 16231	5.00 5.00 5.00	21212	$\begin{array}{c} 16213 \\ 16223 \\ 16233 \end{array}$	\$.00 \$.00 \$.00	$\frac{2}{2}$	$\begin{array}{r} 16214 \\ 16224 \\ 16234 \end{array}$	18.00 18.00 18.00	2 2 2	$\begin{array}{c} 16215 \\ 16225 \\ 16235 \end{array}$	28.00 28.00 28.00	2	15 20 25 1/2	
OLC	$\begin{bmatrix} 1/2 \\ 1/2 \\ 1/2 \\ 1/2 \\ 1 \end{bmatrix}$	$\begin{array}{r} 16901 \\ 14901 \\ 15901 \\ \hline 16911 \end{array}$	$ \begin{array}{r r} 8.20 \\ 12.90 \\ 45.00 \\ \hline 8.20 \end{array} $		$ \begin{array}{r} 16903 \\ 14903 \\ 15903 \\ \hline 16913 \end{array} $	$ \begin{array}{r} 12.30 \\ 17.60 \\ 55.00 \\ \hline 12.30 \end{array} $	4 5	$ \begin{array}{r} 16904 \\ 14904 \\ 15904 \\ \hline 16914 \end{array} $	$\begin{bmatrix} 22.00 \\ 35.00 \\ 65.00 \\ \hline 22.00 \\ \end{bmatrix}$	3	16905 14905 15905 16915	33,00 45,00 80,00 33,00	4 5 3	$\frac{\frac{1/2}{1/2}}{1}$	Type
Type DLC	1 1 2 2	$\begin{array}{r} 14911 \\ 15911 \\ \hline 16921 \\ 14921 \end{array}$	$ \begin{array}{r} 12.90 \\ 45.00 \\ 8.20 \\ 12.90 \end{array} $	$\frac{5}{3}$	$ \begin{array}{r} 14913 \\ 15913 \\ \hline 16923 \\ 14923 \end{array} $	$ \begin{array}{r} 17.60 \\ 55.00 \\ 12.30 \\ 17.60 \end{array} $	5 3	$\begin{array}{ c c c }\hline 14914\\ 15914\\\hline 16924\\ 14924\\\hline\end{array}$	35,00 65,00 22,00 35,00	5 3	$ \begin{array}{r} 14915 \\ 15915 \\ \hline 16925 \\ 14925 \end{array} $	45.00 80.00 33.00 45.00	5 3 4	2 2	Type DLC
	2 5 5	15921 16331 14331	$\begin{array}{r} /45.00 \\ 8.20 \\ 12.90 \end{array}$	$\begin{array}{r} -5 \\ -3 \\ 4 \end{array}$	15923 16333 14333	55.00 12.30 17.60 55.00	5) 3) 4	$\begin{array}{ c c c }\hline 15924\\\hline 16334\\\hline 14334\\\hline 15334\\\hline\end{array}$	65.00 22.00 35.00 65.00	3 4	15925 16335 14335 15335	80.00 33.00 45.00 80.00	3 4	2 5 5 5	
	5 10 10 10	$\begin{array}{r r} 15331 \\ \hline 16351 \\ 14351 \\ 15351 \\ \end{array}$	$ \begin{array}{r r} 45.00 \\ 8.20 \\ 12.90 \\ 45.00 \end{array} $	3 4 5	15333 16353 14353 15353	12.30 17.60 55.00) 3) 4) 5	$\begin{array}{r} 16354 \\ 14354 \\ 15354 \end{array}$	22.00 35.00 65.00	3 4 5	16355 14355 15355	33.00 45.00 80.00) 3) 4) 5	10 10 10	
	15 15 15 20	$ \begin{array}{r r} 16371 \\ 14371 \\ 15371 \\ \hline 16381 \end{array} $	$8.20 \\ 12.90 \\ 45.00 \\ 8.20$	4 5	$ \begin{array}{r} 16373 \\ 14373 \\ 15373 \\ \hline 16383 \end{array} $	$\begin{array}{r} 12.30 \\ 17.60 \\ 55.00 \\ \hline 12.30 \end{array}$	4 5	$ \begin{array}{r} 16374 \\ 14374 \\ 15374 \\ \hline 16384 \end{array} $	$\begin{array}{r} 22.00 \\ 35.00 \\ 65.00 \\ \hline 22.00 \end{array}$	4 5	$ \begin{array}{r} 16375 \\ 14375 \\ 15375 \\ \hline 16385 \end{array} $	33.00 45.00 80.00 33.00) 4) 5	15 15 15 20	_
	20 20 25	$\begin{array}{r r} 14381 \\ 15381 \\ \hline 16391 \end{array}$	$\begin{array}{ c c c }\hline 12.90 \\ 45.00 \\\hline 8.20 \\\hline \end{array}$	4 5 3	14383 15383 16393	17.60 55.00 12.30 17.60	$\begin{array}{c c} 3 & 4 \\ 5 & 5 \\ \hline 3 & 3 \end{array}$	$\begin{array}{r} 14384 \\ 15384 \\ \hline 16394 \\ 14394 \end{array}$	$\begin{array}{r} 35.00 \\ 65.00 \\ \hline 22.00 \\ 35.00 \end{array}$	$\begin{vmatrix} 4\\5\\3 \end{vmatrix}$	$\begin{array}{r} 14385 \\ 15385 \\ \hline 16395 \\ 14395 \end{array}$	45.00 80.00 33.00 45.00	$\frac{1}{0} \frac{5}{3}$	20 20 25 25	
	25 25 30 30	14391 15391 16401 14401	$\begin{array}{r} 12.90 \\ 45.00 \\ \hline 8.20 \\ 12.90 \end{array}$	5 3 1 4	$\begin{array}{r} 14393 \\ 15393 \\ \hline 16403 \\ 14403 \\ \end{array}$	55.00 12.30 17.60	$\begin{array}{c c} 0 & 5 \\ \hline 0 & 3 \\ 0 & 4 \end{array}$	15394 16404 14404	26.00 35.00	$\begin{array}{c c} 0 & 5 \\ \hline 0 & 3 \\ 0 & 4 \end{array}$	15395 16405 14405	38.00 45.00 90.00	$ \begin{array}{c c} 0 & 5 \\ 0 & 3 \\ 0 & 4 \end{array} $	30 30 30 30 30	
Type D	30 40 40 40	15401 16411 14411 15411	45.00 8.20 12.90 45.00) 3) 4	$\begin{array}{r r} 15403 \\ \hline 16413 \\ 14413 \\ 15413 \end{array}$	12.30 17.60 60.00	0 3 0 4	$\begin{array}{r} 15404 \\ \hline 16414 \\ 14414 \\ \hline 15414 \end{array}$	35.00	$\begin{vmatrix} 3\\ 4 \end{vmatrix}$	$\begin{array}{r} 15405 \\ \hline 16415 \\ 14415 \\ 15415 \end{array}$	38.0 45.0 90.0	0 3 0 4 0 5	40 40 40	Type D
E	50 50 50	16421 14421 15421	8.20 12.90 45.00) 4) 5	16423 14423 15423	12.30 17.60 60.00 17.60	$egin{pmatrix} 0 & 4 \ 0 & 5 \end{bmatrix}$	$ \begin{array}{r} 16424\\ 14424\\ 15424\\ \hline 16504 \end{array} $	35.00 75.00	$\begin{array}{ccc} 0 & 4 \\ 0 & 5 \end{array}$	$\begin{array}{r r} & 16425 \\ & 14425 \\ & 15425 \\ \hline & 16505 \end{array}$		$egin{pmatrix} 0 & 4 \ 0 & 5 \end{bmatrix}$	50 50 50 60	
	60 60 75 75	16501 15501 16511 15511	$\frac{45.00}{12.96}$	$\frac{5}{0}$	16503 15503 16513 15513	$\frac{60.0}{17.6}$	$\begin{array}{c c} 0 & 5 \\ \hline 0 & 4 \end{array}$	$ \begin{array}{r} 15504 \\ 15504 \\ 16514 \\ 15514 \end{array} $	80.0 40.0 80.0	0 5 0 4 0 - 5	15505 16515 15515	100.0 50.0 100.0	$egin{array}{ccc} 0 & 5 \ 0 & 4 \ 0 & 5 \ \end{array}$	75 75	
	100 100 150	16521 15521 16531	45.00 16.40	$\begin{array}{c c} 0 & 5 \\ \hline 0 & 4 \end{array}$	16523 15523 16533 15533	$\frac{60.0}{22.3}$	$\begin{array}{c c} 0 & 5 \\ \hline 0 & 4 \end{array}$	16524 15524 16534 15534	$\begin{array}{c c} 80.0 \\ 54.0 \end{array}$	$\begin{array}{c c} 0 & 5 \\ \hline 0 & 4 \end{array}$	$\begin{array}{r r} 16525 \\ 15525 \\ \hline 16535 \\ 15535 \end{array}$	$\frac{100.0}{68.0}$	$\begin{array}{c c} 0 & 5 \\ \hline 0 & 4 \end{array}$	100 100 150 150	
	200 200 200 250	$ \begin{array}{r rrrr} & 15531 \\ & 16541 \\ & 15541 \\ & 16601 \end{array} $	$16.4 \\ 45.0$	$\begin{array}{ccc} 0 & 4 \\ 0 & 5 \end{array}$	$ \begin{array}{r} 10543 \\ \hline 15543 \\ \hline 16603 \end{array} $	22.3 60.0	$\begin{bmatrix} 0 & 4 \\ 0 & 5 \end{bmatrix}$	1654- 1554- 1660-	54.0 85.0	$\begin{array}{c c} 0 & 4 \\ 0 & 5 \end{array}$	16545 15545 16605	68.0 110.0 120.0	00 4 90 5 00 5	200 200 250	******
	300 400	$\frac{16611}{16621}$	48.2	$\begin{array}{c c} 0 & 5 \\ \hline 0 & 5 \end{array}$	16613 16623	$\frac{62.3}{62.3}$	$\frac{ 0 }{ 0 } = \frac{5}{5}$	$-\frac{1661}{1662}$	$\frac{1}{1} = \frac{95.0}{95.0}$	0 5 0 5	16615 16625 Type Letter	120.0	0 5	300 400 tings in l	ight face

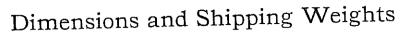
†P. T. is an abbreviation for Potential Transformer Fuse. †See Page 6 for explanation of Type Letters. *Ampere Ratings in light face italics indicate fuses in larger than standard tube size and, therefore, higher than standard interrupting capacity. (See Table, Page 12-A).

The S&C Fuse

Ordering Information—69,000 to 138,000 Volts

The same	*12	69, Rat	,000 Volta ed Volta	ge	92, Ruti	000 Volt ed Voltu	s ge	115. Rate	,000 Volt ed Volta	ito. R	138, Rate	000 Volt d Volta	s s	*Rating	Туре
1 ype	*Ruting Am- peres	Clip	Centers :	4"	Clip	Centers :	30"	Clip	Centers 3	16"	Clip	Centers 4	2"	Am- peres	‡
		Catalog Number	List Price	Tube Size	Catalog Number	List Price	Tube Size	Catalog Number	List Price	Tube Size	Catalog Number	List Price	Tube Size		
	P. T.† 1 2 3	$\begin{array}{r} 16006 \\ 16206 \\ 16216 \\ 16226 \end{array}$	\$18.00 18.00 18.00 18.00	2 2 2 2		S	,,		S			s		P. T.† 1 2 3	Туре
Type B	5 8 10	16236 16246 16256	18.00 22.00 22.00	$egin{array}{c} 2 \\ 2 \\ 2 \\ \hline \ldots \end{array}$										5 8 10	pe B
				- · · · · · · · · · · · · · · · · · · ·											
Type DLC	1 1 1	16916 14916 15916	40.00 55.00 100.00	3 4 5	16917 14917 15917	45.00 65.00 110.00	4	16918 15918	50.00		16919	150.00	5	1 1 1	Type DLC
— E	2 2 2	16926 14926 15926	40,00 55.00 100.00	3 4 5	16927 14927 15927	45.00 65.00 110.00	3 4 5	16928 15928	50.00 130.00	4 5	16929	150.00	5	2 0 0	
	5 5 7 10	16336 14336 15336 16356	40.00 55.00 100.00 40.00	3 4 5 3	16437 14437 15437 16457	45.00 65.00 110.00 45.00	4 5 3	16538 15538 16558	50.00 130.00 50.00	!	16639 16659	150.00 160.00		5 5 10	
	10 10 15 15 15	$\begin{array}{r} 14356 \\ 15356 \\ \hline 16416 \\ 14416 \\ 15416 \\ \end{array}$	55.00 100.00 40.00 55.00 100.00	3 4 5	14457 15457 16477 14477 15477	65.00 110.00 50.00 65.00 110.00	3 4	15558 16578 15578	130.00 70.00 130.00	5 4 5	16679	170.00	5	10 10 15 15 15	
	20 20 20 20	$\begin{array}{r} 16426 \\ 14426 \\ 15426 \end{array}$	40,00 55,00 100,00	3 4 5	16487 14487 15487	50.00 65.00 110.00	3 4 5	16588 15588	70.00 130.00	4 5		170.00		20 20 20	
	25 25 25 30	16436 14436 15436 16446	40.00 55.00 100.00	4 5 3	$\begin{array}{r} 16497 \\ 14497 \\ \hline 15497 \\ \hline 16507 \end{array}$	50.00 65.00 110.00 70.00	4 5	16598 15598 16608	70.00 130.00 130.00	5	16699 16709	170.00		25 25 25 30	
Type D	30 30 40 40	$\begin{array}{r} 14446 \\ 15446 \\ \hline 16456 \\ 14456 \\ \end{array}$	55.00 110.00 50.00 55.00	5 3 4	15507 16517	120.00 70.00	4	16618	130.00	5	16719	180.00	5	30 30 40 40	Type D
•	50 50 50	$\begin{array}{r} 15456 \\ \hline 16466 \\ 14466 \\ 15466 \end{array}$	50.00 55.00 110.00	3 4	15517 16527 15527	$\begin{array}{c} 120.00 \\ \hline 70.00 \\ \hline 120.00 \end{array}$	4	16628	130.00		16729	180.00		40 50 50 50	-
į	60 60 75 75	16506 15506 16516 15516	60.00 120.00 60.00 120.00	- 5 - 4	16607 16617	140.00		16638 	160.00 160.00		16739 16749	190.00		60 60 75 75	
P	100 100 150	$\begin{array}{r} 16526 \\ 16526 \\ 15526 \\ \hline 16536 \end{array}$	60.00 120.00 130.00	4 5	16627 16637	140.00		16658 16668	160.00		16759 16769	190,00 200,00		100 100 150	-
	200 250	16546 16606	130.00		16647	150.00 170.00	. <i></i>	16678	170.00	5	16779	200.00	5	200 250	
	300 400	16616 16626	150.00 150.00	5	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	170.00 170.00	5							300 400	

†P. T. is an abbreviation for Potential Transformer Fuse. ‡See Page 6 for explanation of Type Letters. *Ampere Ratings in light face italies indicate fuses in larger than standard tube size, and, therefore, higher than standard interrupting capacity. (See Table, Page 12-A).



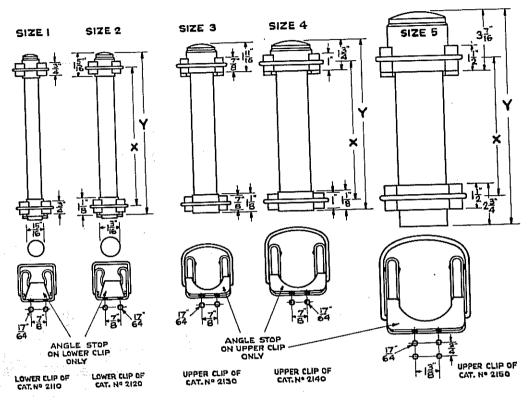


Fig. 20

TVPE	B CON	STRU	CTION	1	TYPE	D (Inc	luding	Type I		OTADY.	RUCTION
	Tobe		Tube S		Tube	Size 3	Tube	Size 4	Tube S	~	Clip Centers
Volts	"Y" Inches	Wt. Lbs. Pkd.	"Y" Inches	Wt. Lbs. Pkd.	"Y" Inches	Wt. Lbs. Pkd.	"Y" Inches	Wt. Lbs. Pkd.	''Y'' Inches	Wt. Lbs. Pkd.	Tube Sizes
7,500 23,000 34,500 46,000	9 5/6 12 ¹³ /6 16 5/6 19 5/6	1½ 1¾ 1¾ 2 2¼	9 ½6 12 ¹³ 6 16 ½6 19 ½6	$rac{2}{2^{1/8}} \ 2^{1/4} \ 2^{5/8}$	911.6 13 \$6 1611.6 1911.6	3½ 4 4½ 5	$9\frac{1}{4}$ $13\frac{1}{4}$ $16\frac{1}{4}$ $19\frac{3}{4}$	6 7 8 9	$\begin{array}{c} 125\% \\ 161\% \\ 195\% \\ 225\% \end{array}$	18 24 30 36	8" 11½" 15" 18"
69,000 92,000 115,000	10 716	, , , , , , ,	25 5/6	31/4	25 ¹¹ / ₁₆ 31 ¹¹ / ₁₆	$ \begin{array}{c} $	25¾ 31¾ 37¾	12 . 21 . 30	285/s 345/s 405/s 465/s	50 70 85 100	24" 30" 36" 42"

S&C Fuse Clips

Catalog	Type of Fusc	Fuse Tube Size (See pages 14 and 15)	List Price Per Pair
Number		1	\$1.00
2110	В		1.00
2120	В		2.00
2130	D or DLC	3	2,50
2140	D or DLC	4	
2150	D or DLC	5	6.00
2100			

S&C Fuse Tongs

For the placing and removal of fuses, two types of Fuse Tongs, shown below, are offered. These tongs are made of seasoned hard wood, kiln dried, and given special treatment and finish to prevent moisture absorption.

The Type H is for use where the operator is at the approximate height of the fuse and can handle it with tongs which hold the fuse at a 90° angle with the handles. Quite often, however, the fuse is mounted above the operator, in which case the Type HA Tongs are better used. In cases where the fuse is mounted at a considerable height, the "Pole-Pull" Fuse Mountings on the following page offer the easiest method of inserting or removing a fuse.

Take 4 Sizes of Fuses

The size limit of fuses which it is possible to handle with these tongs will depend somewhat on the ability of the operator and the location of the fuse. However, the tongs will tightly grip S & C Fuses of the Nos. 1, 2, 3 and 4 sizes, dimensions of which are given on page 16. Size 5 fuses cannot be handled with tongs. For method of handling Size 5 fuses up to 34500 volts see "Pole-Pull" Fuse Mountings described on the following page.

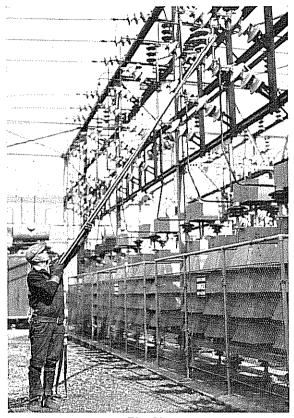
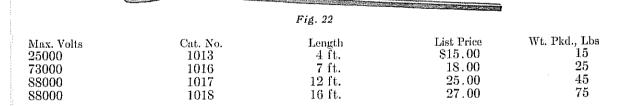


Fig. 21

Type H Fuse Tongs (90°)



Type HA Fuse Tongs (45°)

		Fig. 22A		
Max. Volts	Cat. No.	Length 4 ft. 7 ft. 12 ft. 16 ft.	List Price	Wt. Pkd., Lbs.
25000	1023		\$16.00	15
73000	1026		19.00	25
88000	1027		26.00	45
88000	1028		28.00	75

Page 17

"Pole-Pull" Fuse Mounting primarily for high mounting of S&C Fuses

Where fuses are mounted at a considerable height above the ground the usual method of handling them with tongs is difficult and the "Pole-Pull" Fuse Mounting is offered to The "Pole-Pull" Fuse Mounting, in types for either indoor or outdoor installations, is listed in Bulletins 200J and 200R.

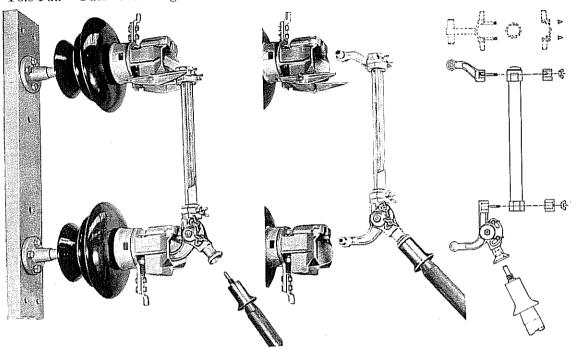


Fig. 23-Showing "Pole-Pull" Fuse Mounting as in Service.
Pole ready to enter socket.

provide a practical means for changing fuses

when they are mounted in high positions.

The "Pole-Pull" Fuse Mounting accomodates sizes 3 and 4 S&C Fuses up to 115,000 volts and size 5 S&C Fuses up to 34500 volts. It consists of the usual steel base and insulators with a set of contact clips of special design into which fit a set of contact terminals clamped to a standard S&C Fuse. contact terminals slide easily into, or out of, the special contact clips. The fuse is handled by means of a treated wood pole having a coarsely threaded stud which screws into a socket at the lower end of the fuse. The angle of the socket is adjustable to meet the requirements of each installation.

The contact terminals, including clamps, although ample, both electrically and mechanically, are very light in weight, and the total weight handled at the end of the pole is very little more than the weight of the fuse alone.

Fig. 24—Showing Pole At-tached and Contactors withdrawn from clips

Fig. 25-Showing S&C Fuse Removed from Fuse-Ferrule Clamps

(Patent Pending)

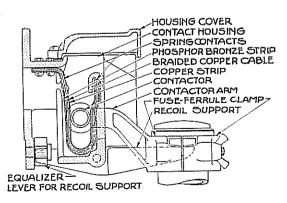


Fig. 26—Showing Details of the well housed contact Clip of the "Pole-Pull" Fuse Mounting

For Distribution Circuits

For application on distribution circuits, the S&C Fuse is also supplied with a weatherproof,

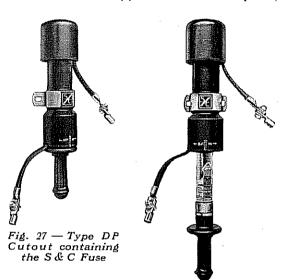


Fig. 32—Showing how the Fuse is removed from the Cutout by means of the Insulated Handle to which Fuse is attached

insulating housing, and this arrangement is called the Type DP Cutout. It is principally applied on 2200 to 6600 volt systems for primary protection on distribution transformers of 50 to 300 KVA capacity.

Type DP Cutout

This cutout consists of a special form of the S&C Fuse, designed for attachment to an insulated handle and for inserting in a weather proof, insulating housing. This housing contains adequate self-aligning contact clips to which are connected the flexible leads appearing in the illustration.

The complete cutout occupies a space of only 5"x5"x21" and makes possible an unusually neat appearing installation.

Fuses for the Type DP Cutout are rated at 10, 20, 30, 40, 50, 60, 75, 100, 150 and 200 amperes.

High Interrupting Capacity

Numerous tests and wide use under service conditions have shown the interrupting capacity of the Type DP Cutout to be approximately 10,000 amperes at 2300-4000 volts.

Bulletin 201A gives complete information, and will be gladly supplied on request.

A Sturdy Convenient Carton

S&C Fuses of the smaller and medium sizes are packed for stocking in a strong cylindrical carton and labeled on the outside with the ampere and voltage ratings for quick identification.

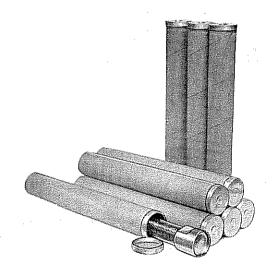


Fig. 28—Cartons in which S & C Fuses are packed

Keep the Container

Users are urged to preserve these containers in their fuse stockroom or other convenient location where they will be easily available for repacking S & C Fuses when returning them to the factory for refilling. Thus returns of blown fuses will be made with facility and at the lowest packing cost.

The S&C Fuse for Load Breaking

How to Interrupt Load Currents in Switch Operation, with the S & C Fuse, and Save the Cost of an Oil Circuit-Breaker

A Money Saving Arrangement

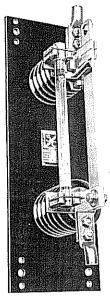


Fig. 29—Type YB Fuse-Break, Load-Interrupting Switch for Indoor Service. Patented

There are numerous places in every large generating or distributing system where it is desirable to have a simple means of interrupting load currents, at moderate and high voltage, without the use of an expensive oil circuit breaker. Where opening of the circuit is infrequent, this is conveniently accomplished at a great saving over the cost of an oil circuit breaker, by using the S & C, Type YB, Fuse-Break, Load-Interrupting Switch.

One form of this switch is shown in Fig. 29. It consists of a disconnecting switch arranged so that the blade is shunted by an S&C Fuse of low ampere rating. When the fuse is out of the clips the switch blade is locked in the closed position, but the in-

serting of the fuse releases the lock for the opening of the blade. The close up view of the top section of the switch, Fig. 30, shows the blade locked when the fuse is removed.

How It Operates

To interrupt a load the S&C Fuse is first inserted in the clips and then the disconnecting

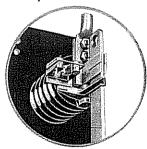


Fig. 30—Showing how the Switch Blade is locked until a Fuse is placed in the Fuse Clips

switch blade is opened rapidly. An are is thereby drawn between the blade and the contact clip at the instant the blade leaves the clip.

The voltage maximum across the arc cannot exceed the product of the current in the circuit and the resistance of the fuse. This voltage is very small, being in the order of approximately 100 volts when interrupting a 200 ampere load. The arc quickly becomes unstable, due to the transfer of current to the fuse, and is extinguished as it is lengthened by the movement of the switch blade away from the clip. The extinction of the arc is followed by the blowing of the fuse which opens the circuit.

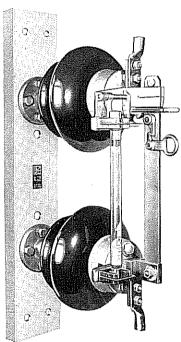


Fig. 31—Type YB Fuse-Break, Load-Interrupting Switch for Outdoor Service. Patented

Many Possible Applications

Another form of the YB Fuse-Break Load-Interrupting Switch is shown in Fig. 31. This form has an extra lock on the switch blade, which locks the switch blade in the closed position until released by a downward pull with a switch stick.

The possible applications of the YB Fuse-Break Load-Interrupting Switch are many and varied. Correspondence on this subject is invited, and recommendations and quotations will be made on request.

Many in Use

The YB Fuse-Break Load-Interrupting Switch has been time-tried-and-tested and is giving satisfactory service. More than four hundred are in use on one system.



TRADE MAIK BEG. U. S. PAT. DFF.